

# Dual and Quad 250μA, 3MHz, 200V/μs **Operational Amplifiers**

### FEATURES

- 3MHz Gain Bandwidth
- 200V/us Slew Rate
- 250µA Supply Current per Amplifier
- C-Load<sup>TM</sup> Op Amp Drives All Capacitive Loads
- Unity-Gain Stable
- Maximum Input Offset Voltage: 600μV
- Maximum Input Bias Current: 50nA
- Maximum Input Offset Current: 15nA
- Minimum DC Gain, R<sub>1</sub> = 2k: 30V/mV
- Input Noise Voltage: 14nV/√Hz
- Settling Time to 0.1%, 10V Step: 700ns
- Settling Time to 0.01%, 10V Step: 1.25µs
- Minimum Output Swing into 1k: ±13V
- Minimum Output Swing into  $500\Omega$ :  $\pm 3.4V$
- Specified at  $\pm 2.5$ V,  $\pm 5$ V and  $\pm 15$ V

### **APPLICATIONS**

- Battery-Powered Systems
- Wideband Amplifiers
- **Buffers**
- Active Filters
- **Data Acquisition Systems**
- Photodiode Amplifiers

### DESCRIPTION

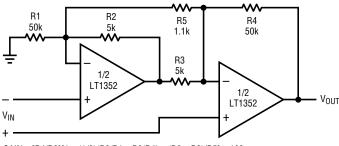
The LT®1352/LT1353 are dual and quad, very low power, high speed operational amplifiers with outstanding AC and DC performance. The amplifiers feature much lower supply current and higher slew rate than devices with comparable bandwidth. The circuit combines the slewing performance of a current feedback amplifier in a true operational amplifier with matched high impedance inputs. The high slew rate ensures that the large-signal bandwidth is not degraded. Each output is capable of driving a  $1k\Omega$  load to  $\pm 13V$  with  $\pm 15V$  supplies and a  $500\Omega$  load to  $\pm 3.4V$  on ±5V supplies.

The LT1352/LT1353 are members of a family of fast, high performance amplifiers using this unique topology and employing Linear Technology Corporation's advanced complementary bipolar processing. For higher bandwidth devices with higher supply current see the LT1354 through LT1365 data sheets. Bandwidths of 12MHz, 25MHz, 50MHz and 70MHz are available with 1mA, 2mA, 4mA and 6mA of supply current per amplifier. Singles, duals and quads of each amplifier are available.

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## TYPICAL APPLICATION

#### **Instrumentation Amplifier**

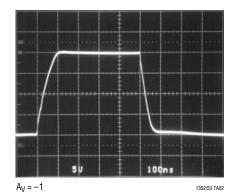


1352/53 TA01

 $\mathsf{GAIN} = [\mathsf{R4/R3}][1 + (1/2)(\mathsf{R2/R1} + \mathsf{R3/R4}) + (\mathsf{R2} + \mathsf{R3})/\mathsf{R5}] = 102$ TRIM R5 FOR GAIN

TRIM R1 FOR COMMON MODE REJECTION

#### Large-Signal Response

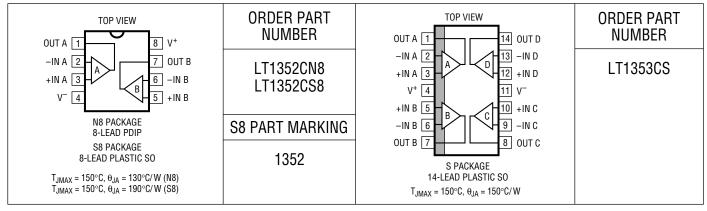


## **ABSOLUTE MAXIMUM RATINGS**

Total Supply Voltage (V + to V -)	36V
Differential Input Voltage	±10V
Input Voltage	±V <sub>S</sub>
Output Short-Circuit Duration (Note 1)	Indefinite
Operating Temperature Range	-40°C to 85°C

Specified Temperature Range	. −40°C to 85°C
Maximum Junction Temperature (See B	Below)
Plastic Package	150°C
Storage Temperature Range	-65°C to 150°C
Lead Temperature (Soldering, 10 sec)	300°C

# PACKAGE/ORDER INFORMATION



Consult factory for Industrial and Military grade parts.

# **ELECTRICAL CHARACTERISTICS** $T_A = 25^{\circ}C$ , $V_{CM} = 0V$ unless otherwise noted.

SYMBOL	PARAMETER	CONDITIONS	VSUPPLY	MIN	TYP	MAX	UNITS
V <sub>0S</sub>	Input Offset Voltage		±15V ±5V		0.2 0.2	0.6 0.6	mV mV
			±2.5V		0.2	0.8	mV
I <sub>0S</sub>	Input Offset Current		±2.5V to ±15V		5	15	nA
I <sub>B</sub>	Input Bias Current		±2.5V to ±15V		20	50	nA
e <sub>n</sub>	Input Noise Voltage	f = 10kHz	±2.5V to ±15V		14		nV/√Hz
in	Input Noise Current	f = 10kHz	±2.5V to ±15V		0.5		pA/√Hz
R <sub>IN</sub>	Input Resistance	V <sub>CM</sub> = ±12V Differential	±15V ±15V	300	600 20		MΩ MΩ
C <sub>IN</sub>	Input Capacitance		±15V		3		pF
	Positive Input Voltage Range		±15V ±5V ±2.5V	12.0 2.5 0.5	13.5 3.5 1.0		V V V
	Negative Input Voltage Range		±15V ±5V ±2.5V		-13.5 -3.5 -1.0	-12.0 -2.5 -0.5	V V V
CMRR	Common Mode Rejection Ratio	$V_{CM} = \pm 12V$ $V_{CM} = \pm 2.5V$ $V_{CM} = \pm 0.5V$	±15V ±5V ±2.5V	80 78 68	94 86 77		dB dB dB
PSRR	Power Supply Rejection Ratio	$V_S = \pm 2.5 V \text{ to } \pm 15 V$		90	106		dB

# **ELECTRICAL CHARACTERISTICS** $T_A = 25^{\circ}C$ , $V_{CM} = 0V$ unless otherwise noted.

SYMBOL	PARAMETER	CONDITIONS	V <sub>SUPPLY</sub>	MIN	TYP	MAX	UNITS
A <sub>VOL</sub>	Large-Signal Voltage Gain	$V_{OUT} = \pm 12V, R_L = 5k$ $V_{OUT} = \pm 10V, R_1 = 2k$	±15V ±15V	40 30	80 60		V/mV V/mV
		$V_{OUT} = \pm 10V, R_L = 1k$	±15V	20	40		V/mV
		$V_{OUT} = \pm 2.5V, R_L = 5k$	±5V	30	60		V/mV
		$V_{OUT} = \pm 2.5V, R_L = 2k$	±5V	25	50		V/mV
		$V_{OUT} = \pm 2.5V, R_L = 1k$	±5V	15	30		V/mV
		$V_{OUT} = \pm 1V$ , $R_L = 5k$	±2.5V	20	40		V/mV
$V_{OUT}$	Output Swing	$R_L = 5k, V_{IN} = \pm 10mV$	±15V	13.5	14.0		±V
		$R_L = 2k$ , $V_{IN} = \pm 10mV$	±15V	13.4	13.8		±V
		$R_L = 1k$ , $V_{IN} = \pm 10mV$	±15V	13.0	13.4		±V
		$R_L = 1k, V_{IN} = \pm 10mV$	±5V	3.5	4.0		±V
		$R_L = 500\Omega$ , $V_{IN} = \pm 10$ mV	±5V	3.4	3.8		±V
		$R_L = 5k$ , $V_{IN} = \pm 10mV$	±2.5V	1.3	1.7		±V
I <sub>OUT</sub>	Output Current	$V_{OUT} = \pm 13V$	±15V	13.0	13.4		mA
		$V_{OUT} = \pm 3.4V$	±5V	6.8	7.6		mA
I <sub>SC</sub>	Short-Circuit Current	$V_{OUT} = 0V$ , $V_{IN} = \pm 3V$	±15V	30	45		mA
SR	Slew Rate	$A_V = -1$ , $R_L = 5k$ (Note 2)	±15V	120	200		V/µs
			±5V	30	50		V/µs
	Full-Power Bandwidth	10V Peak (Note 3)	±15V		3.2		MHz
		3V Peak (Note 3)	±5V		2.6		MHz
GBW	Gain Bandwidth	f = 200kHz, R <sub>L</sub> = 10k	±15V	2.0	3.0		MHz
			± 5V	1.8	2.7		MHz
			± 2.5V		2.5		MHz
$t_r$ , $t_f$	Rise Time, Fall Time	$A_V = 1$ , 10% to 90%, 0.1V	±15V		46		ns
			±5V		53		ns
	Overshoot	$A_V = 1, 0.1V$	±15V		13		%
			±5V		16		%
	Propagation Delay	50% V <sub>IN</sub> to 50% V <sub>OUT</sub> , 0.1V	±15V		41		ns
			±5V		52		ns
$\overline{t_s}$	Settling Time	10V Step, 0.1%, A <sub>V</sub> = −1	±15V		700		ns
•		10V Step, 0.01%, $A_V = -1$	±15V		1250		ns
		5V Step, 0.1%, $A_V = -1$	±5V		950		ns
		5V Step, 0.01%, $A_V = -1$	±5V		1400		ns
$R_0$	Output Resistance	$A_V = 1$ , $f = 20kHz$	±15V		1.5		Ω
	Channel Separation	$V_{OUT} = \pm 10V$ , $R_L = 2k$	±15V	101	120		dB
I <sub>S</sub>	Supply Current	Each Amplifier	±15V		250	320	μА
		Each Amplifier	±5V		230	300	μΑ

# $0^{\circ}C \leq T_{A} \leq 70^{\circ}C, \; V_{CM}$ = 0V unless otherwise noted.

SYMBOL	PARAMETER	CONDITIONS	V <sub>SUPPLY</sub>	MIN	TYP	MAX	UNITS
$\overline{V_{0S}}$	Input Offset Voltage		±15V			0.8	mV
			±5V			8.0	mV
			±2.5V			1.0	mV
	Input V <sub>OS</sub> Drift	(Note 4)	±2.5V to ±15V		3	8	μV/°C
I <sub>OS</sub>	Input Offset Current		±2.5V to ±15V			20	nA
I <sub>B</sub>	Input Bias Current		±2.5V to ±15V			75	nA



# **ELECTRICAL CHARACTERISTICS** $0^{\circ}C \le T_A \le 70^{\circ}C$ , $V_{CM}$ = 0V unless otherwise noted.

SYMBOL	PARAMETER	CONDITIONS	V <sub>SUPPLY</sub>	MIN	TYP	MAX	UNITS
CMRR	Common Mode Rejection Ratio	$V_{CM} = \pm 12V$	±15V	78			dB
		$V_{CM} = \pm 2.5V$	±5V	77			dB
		$V_{CM} = \pm 0.5V$	±2.5V	67			dB
PSRR	Power Supply Rejection Ratio	$V_S = \pm 2.5 V \text{ to } \pm 15 V$		89			dB
$A_{VOL}$	Large-Signal Voltage Gain	$V_{OUT} = \pm 12V, R_L = 5k$	±15V	25			V/mV
		$V_{OUT} = \pm 10V, R_L = 2k$	±15V	20			V/mV
		$V_{OUT} = \pm 2.5V, R_L = 5k$	±5V	20			V/mV
		$V_{OUT} = \pm 2.5V, R_L = 2k$	±5V	15			V/mV
		$V_{OUT} = \pm 2.5V, R_L = 1k$	±5V	10			V/mV
		$V_{OUT} = \pm 1V, R_L = 5k$	±2.5V	15			V/mV
$V_{OUT}$	Output Swing	$R_L = 5k$ , $V_{IN} = \pm 10mV$	±15V	13.4			±V
		$R_L = 2k, V_{IN} = \pm 10mV$	±15V	13.3			±V
		$R_L = 1k, V_{IN} = \pm 10mV$	±15V	12.0			±V
		$R_L = 1k, V_{IN} = \pm 10mV$	±5V	3.4			±V
		$R_L = 500\Omega$ , $V_{IN} = \pm 10$ mV	±5V	3.3			±V
		$R_L = 5k$ , $V_{IN} = \pm 10mV$	±2.5V	1.2			±V
I <sub>OUT</sub>	Output Current	$V_{OUT} = \pm 12V$	±15V	12.0			mA
		$V_{OUT} = \pm 3.3V$	±5V	6.6			mA
$I_{SC}$	Short-Circuit Current	$V_{OUT} = 0V$ , $V_{IN} = \pm 3V$	±15V	24			mA
SR	Slew Rate	$A_V = -1$ , $R_L = 5k$ (Note 2)	±15V	100			V/µs
			±5V	21			V/µs
GBW	Gain Bandwidth	f = 200kHz, R <sub>I</sub> = 10k	±15V	1.8			MHz
		_	± 5V	1.6			MHz
	Channel Separation	$V_{OUT} = \pm 10V, R_L = 2k$	±15V	100			dB
Is	Supply Current	Each Amplifier	±15V			350	μΑ
-		Each Amplifier	±5V			330	μΑ

### $-40^{\circ}C \leq T_{A} \leq 85^{\circ}C,~V_{CM}$ = OV unless otherwise noted (Note 5).

SYMBOL	PARAMETER	CONDITIONS	V <sub>SUPPLY</sub>	MIN	TYP	MAX	UNITS
$\overline{V_{0S}}$	Input Offset Voltage		±15V			1.0	mV
			±5V			1.0	mV
			±2.5V			1.2	mV
	Input V <sub>OS</sub> Drift	(Note 4)	±2.5V to ±15V		3	8	μV/°C
I <sub>OS</sub>	Input Offset Current		±2.5V to ±15V			30	nA
I <sub>B</sub>	Input Bias Current		±2.5V to ±15V			100	nA
CMRR	Common Mode Rejection Ratio	$V_{CM} = \pm 12V$	±15V	76			dB
		$V_{CM} = \pm 2.5V$	±5V	76			dB
		$V_{CM} = \pm 0.5V$	±2.5V	66			dB
PSRR	Power Supply Rejection Ratio	$V_S = \pm 2.5 V \text{ to } \pm 15 V$		87			dB
A <sub>VOL</sub>	Large-Signal Voltage Gain	$V_{OUT} = \pm 12V, R_L = 5k$	±15V	20			V/mV
		$V_{OUT} = \pm 10V, R_L = 2k$	±15V	15			V/mV
		$V_{OUT} = \pm 2.5V, R_L = 5k$	±5V	15			V/mV
		$V_{OUT} = \pm 2.5V, R_L = 2k$	±5V	10			V/mV
		$V_{OUT} = \pm 2.5V, R_L = 1k$	±5V	8			V/mV
		$V_{OUT} = \pm 1V, R_L = 5k$	±2.5V	10			V/mV

# **ELECTRICAL CHARACTERISTICS** $-40^{\circ}C \le T_{A} \le 85^{\circ}C$ , $V_{CM}$ = 0V unless otherwise noted (Note 4).

SYMBOL	PARAMETER	CONDITIONS	V <sub>SUPPLY</sub>	MIN	TYP	MAX	UNITS
V <sub>OUT</sub>	Output Swing	$R_L = 5k, V_{IN} = \pm 10mV$	±15V	13.3			±V
		$R_L = 2k, V_{IN} = \pm 10mV$	±15V	13.2			±V
		$R_L = 1k, V_{IN} = \pm 10mV$	±15V	10.0			±V
		$R_L = 1k, V_{IN} = \pm 10mV$	±5V	3.3			±V
		$R_L = 500\Omega$ , $V_{IN} = \pm 10$ mV	±5V	3.2			±V
		$R_L = 5k, V_{IN} = \pm 10mV$	±2.5V	1.1			±V
I <sub>OUT</sub>	Output Current	$V_{OUT} = \pm 10V$	±15V	10.0			mA
00.		$V_{OUT} = \pm 3.2V$	±5V	6.4			mA
I <sub>SC</sub>	Short-Circuit Current	$V_{OUT} = 0V$ , $V_{IN} = \pm 3V$	±15V	20			mA
SR	Slew Rate	$A_V = -1$ , $R_L = 5k$ (Note 2)	±15V	50			V/µs
			±5V	15			V/µs
GBW	Gain Bandwidth	f = 200kHz, R <sub>1</sub> = 10k	±15V	1.6			MHz
		_	± 5V	1.4			MHz
	Channel Separation	$V_{OUT} = \pm 10V, R_L = 2k$	±15V	99			dB
Is	Supply Current	Each Amplifier	±15V			380	μА
		Each Amplifier	±5V			350	μA

**Note 1:** A heat sink may be required to keep the junction temperature below absolute maximum when the output is shorted indefinitely.

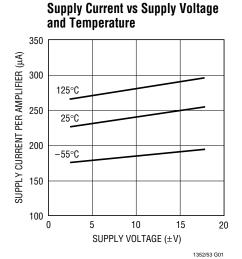
**Note 2:** Slew rate is measured between  $\pm 8V$  on the output with  $\pm 12V$  input for  $\pm 15V$  supplies and  $\pm 2V$  on the output with  $\pm 3V$  input for  $\pm 5V$  supplies.

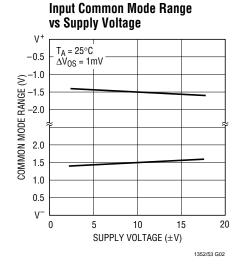
**Note 3:** Full-power bandwidth is calculated from the slew rate measurement: FPBW = (Slew Rate)/ $2\pi V_P$ .

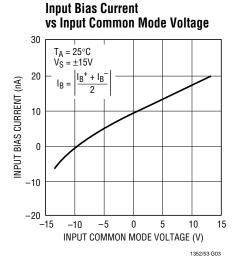
Note 4: This parameter is not 100% tested.

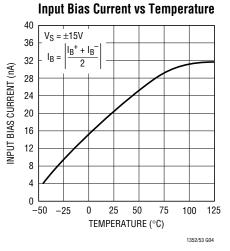
**Note 5:** The LT1352/LT1353 are designed, characterized and expected to meet these extended temperature limits, but are not tested at  $-40^{\circ}$ C and 85°C. Guaranteed I grade parts are available, consult factory.

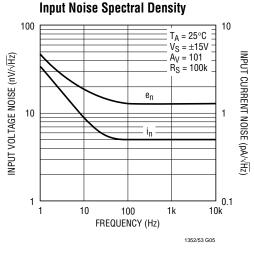
# TYPICAL PERFORMANCE CHARACTERISTICS

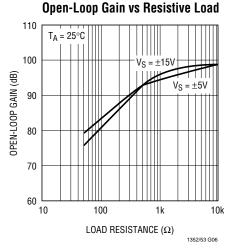


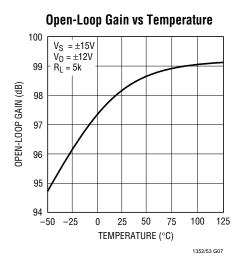


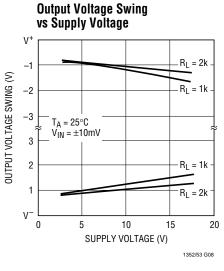


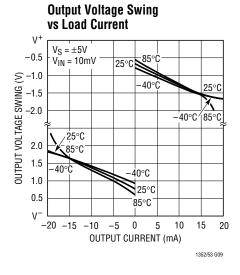


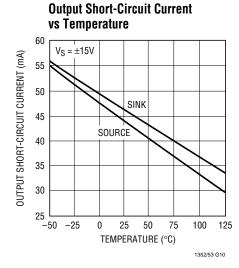


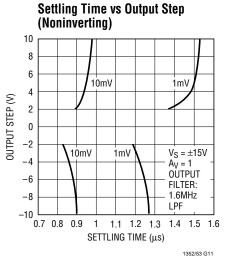


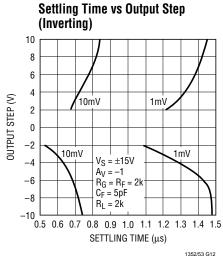


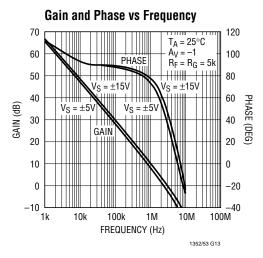


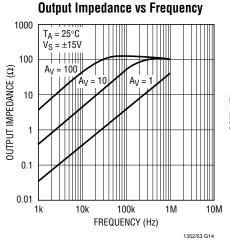


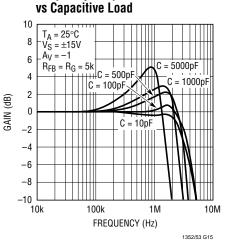






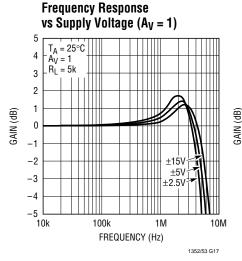


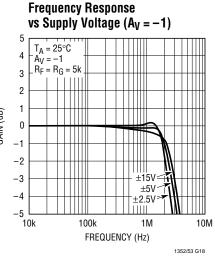


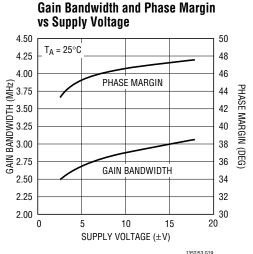


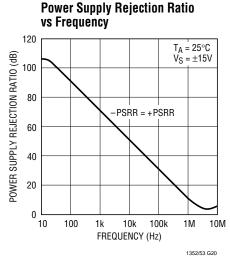
**Frequency Response** 

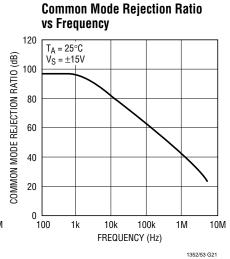
Gain Bandwidth and Phase Margin vs Temperature 50 4.50  $V_S = \pm 15V$ 48 4.25  $V_S = \pm 5V$ 4.00 46 ¥ 3.75 PHASE MARGIN 44 PHASE MARGIN (DEG 3.50 3.25 3.00 2.75 42 40 **GAIN BANDWIDTH** 38  $V_S = \pm 15V$ 36 2.50 34  $V_S = \pm 5V$ 32 2.25 30 125 -50 -25 0 25 50 75 100 TEMPERATURE (°C)



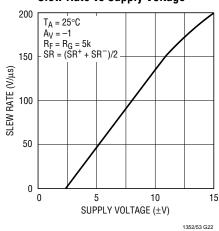




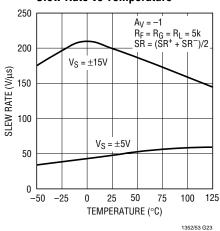




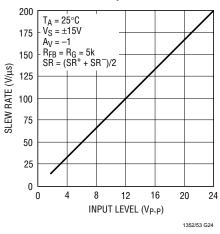
### **Slew Rate vs Supply Voltage**



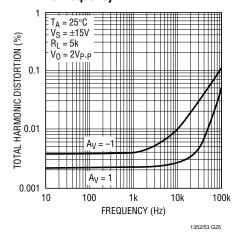
#### Slew Rate vs Temperature



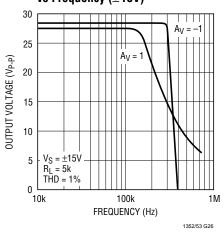
#### Slew Rate vs Input Level



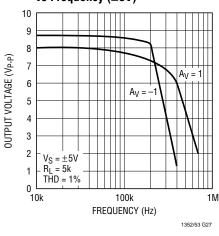
# Total Harmonic Distortion vs Frequency



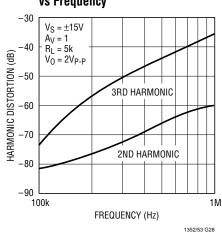
# Undistorted Output Swing vs Frequency $(\pm 15V)$



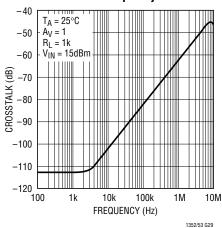
# Undistorted Output Swing vs Frequency $(\pm 5V)$



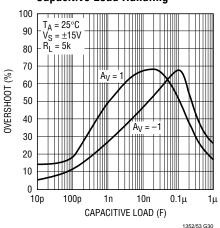
# 2nd and 3rd Harmonic Distortion vs Frequency



#### Crosstalk vs Frequency

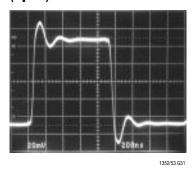


#### **Capacitive Load Handling**

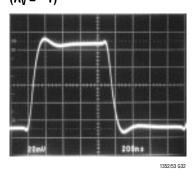


1352/53 G3

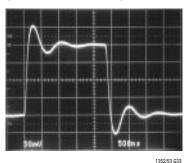
Small-Signal Transient  $(A_V = 1)$ 



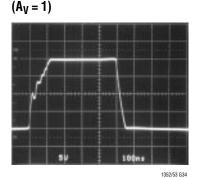
Small-Signal Transient  $(A_V = -1)$ 



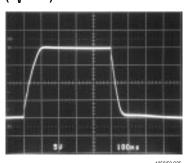
Small-Signal Transient  $(A_V = -1, C_L = 1000pF)$ 



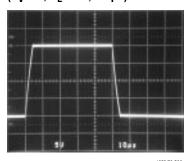
Large-Signal Transient



Large-Signal Transient  $(A_V = -1)$ 



Large-Signal Transient  $(A_V = 1, C_L = 10,000pF)$ 



# APPLICATIONS INFORMATION

### **Layout and Passive Components**

The LT1352/LT1353 amplifiers are easy to use and tolerant of less than ideal layouts. For maximum performance (for example, fast 0.01% settling) use a ground plane, short lead lengths and RF-quality bypass capacitors (0.01 $\mu$ F to 0.1 $\mu$ F). For high drive current applications use low ESR bypass capacitors (1 $\mu$ F to 10 $\mu$ F tantalum).

The parallel combination of the feedback resistor and gain setting resistor on the inverting input can combine with the input capacitance to form a pole which can cause peaking or even oscillations. If feedback resistors greater than 10k are used, a parallel capacitor of value,  $C_F > (R_G)(C_{IN}/R_F)$ , should be used to cancel the input pole and optimize dynamic performance. For applications where the DC noise gain is one and a large feedback resistor is used,  $C_F$  should be greater than or equal to  $C_{IN}$ . An example would be an I-to-V converter as shown in the Typical Applications section.

### **Capacitive Loading**

The LT1352/LT1353 are stable with any capacitive load. As the capacitive load increases, both the bandwidth and phase margin decrease so there will be peaking in the frequency domain and in the transient response. Graphs of Frequency Response vs Capacitive Load, Capacitive Load Handling and the transient response photos clearly show these effects.

### **Input Considerations**

Each of the LT1352/LT1353 amplifier inputs is the base of an NPN and PNP transistor whose base currents are of opposite polarity and provide first order bias current cancellation. Because of variation in the matching of NPN and PNP beta, the polarity of the input current can be positive or negative. The offset current does not depend on NPN to PNP beta matching and is well controlled. The use of balanced source resistance at each input is recom-



### APPLICATIONS INFORMATION

mended for applications where DC accuracy must be maximized. The inputs can withstand differential input voltages of up to 10V without damage and need no clamping or source resistance for protection. Differential inputs generate large supply currents (up to 40mA) as required for high slew rates. Typically power dissipation does not significantly increase because of the low duty cycle of the transient inputs. If the device is used as a comparator with sustained differential inputs, excessive power dissipation may result.

### **Circuit Operation**

The LT1352/LT1353 circuit topology is a true voltage feedback amplifier that has the slewing behavior of a current feedback amplifier. The operation of the circuit can be understood by referring to the Simplified Schematic.

The inputs are buffered by complementary NPN and PNP emitter followers which drive R1, a 1k resistor. The input voltage appears across the resistor generating currents which are mirrored into the high impedance node and compensation capacitor  $C_T$ . Complementary followers form an output stage which buffers the gain node from the load. The output devices Q19 and Q22 are connected to form a composite PNP and a composite NPN.

The bandwidth is set by the input resistor and the capacitance on the high impedance node. The slew rate is determined by the current available to charge the high impedance node capacitance. This current is the differential input voltage divided by R1, so the slew rate is proportional to the input. Highest slew rates are therefore seen in the lowest gain configurations. For example, a 10V output step in a gain of 10 has only a 1V input step whereas the same output step in unity gain has a 10 times greater input step. The graph Slew Rate vs Input Level illustrates this relationship. In higher gain configurations the large-signal performance and the small-signal performance both look like a single pole response.

Capacitive load compensation is provided by the  $R_{C}$ ,  $C_{C}$  network which is bootstrapped across the output stage. When the amplifier is driving a light load the network has no effect. When driving a capacitive load (or a low value resistive load) the network is incompletely bootstrapped and adds to the compensation at the high impedance node. The added capacitance slows down the amplifier and a zero is created by the RC combination, both of which improve the phase margin. The design ensures that even for very large load capacitances, the total phase lag can never exceed 180 degrees (zero phase margin) and the amplifier remains stable.

### **Power Dissipation**

The LT1352/LT1353 combine high speed and large output drive in small packages. Because of the wide supply voltage range, it is possible to exceed the maximum junction temperature of 150°C under certain conditions. Maximum junction temperature  $T_J$  is calculated from the ambient temperature  $T_A$  and power dissipation  $P_D$  as follows:

LT1352CN8:  $T_J = T_A + (P_D)(130^{\circ}C/W)$ LT1352CS8:  $T_J = T_A + (P_D)(190^{\circ}C/W)$ LT1353CS:  $T_J = T_A + (P_D)(150^{\circ}C/W)$ 

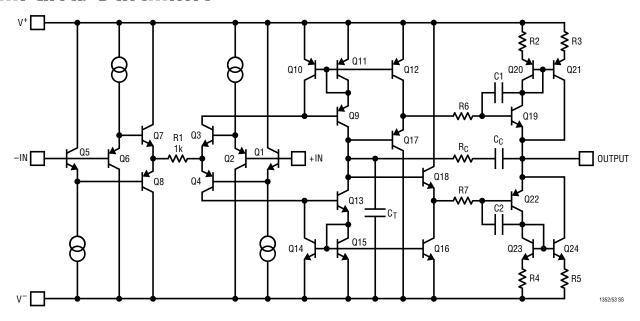
Worst-case power dissipation occurs at the maximum supply current and when the output voltage is at 1/2 of either supply voltage (or the maximum swing if less than 1/2 supply voltage). For each amplifier P<sub>D(MAX)</sub> is:

$$P_{D(MAX)} = (V^{+} - V^{-})(I_{S(MAX)}) + (V^{+}/2)^{2}/R_{L} \text{ or } (V^{+} - V^{-})(I_{S(MAX)}) + (V^{+} - V_{MAX})(I_{MAX})$$

Example: LT1353 in S14 at 85°C,  $V_S = \pm 15V$ ,  $R_L = 500\Omega$ ,  $V_{OUT} = \pm 5V$  ( $\pm 10$ mA)

 $P_{D(MAX)} = (30V)(380\mu A) + (15V - 5V)(10mA) = 111mW$  $T_{J} = 85^{\circ}C + (4)(111mW)(150^{\circ}C/W) = 152^{\circ}C$ 

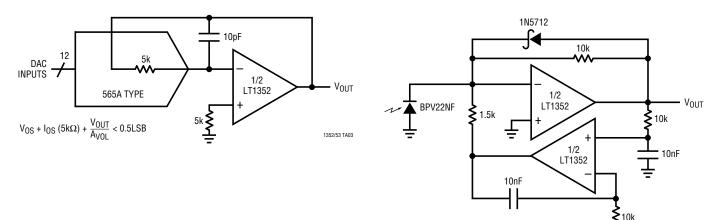
# SIMPLIFIED SCHEMATIC



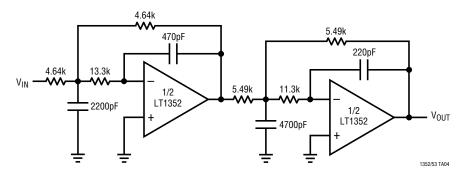
# TYPICAL APPLICATIONS

DAC I-to-V Converter

### 400kHz Photodiode Preamp with 10kHz Highpass Loop



#### 20kHz, 4th Order Butterworth Filter



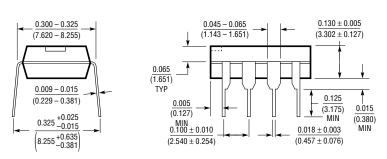


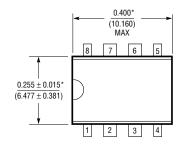
1352/53 TA05

# PACKAGE DESCRIPTION Dimensions in inches (millimeters) unless otherwise noted.

### **N8 Package** 8-Lead PDIP (Narrow 0.300)

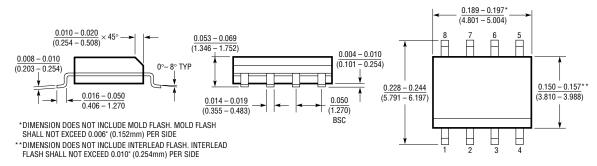
(LTC DWG # 05-08-1510)



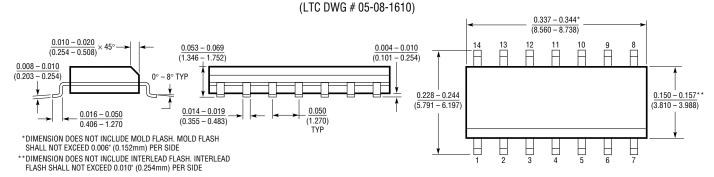


### S8 Package 8-Lead Plastic Small Outline (Narrow 0.150)

(LTC DWG # 05-08-1610)



### S Package 14-Lead Plastic Small Outline (Narrow 0.150)



# **RELATED PARTS**

PART NUMBER	DESCRIPTION	COMMENTS
LT1351	250μA, 3MHz, 200V/μs Op Amp	Good DC Precision, C-Load Stable, Power Saving Shutdown
LT1354/55/56	Single/Dual/Quad 1mA, 12MHz, 400V/µs Op Amp	Good DC Precision, Stable with All Capacitive Loads

<sup>\*</sup>THESE DIMENSIONS DO NOT INCLUDE MOLD FLASH OR PROTRUSIONS. MOLD FLASH OR PROTRUSIONS SHALL NOT EXCEED 0.010 INCH (0.254mm)